

$$\vec{F}_{\text{tot}} = \sum_{\mu} A_{\mu} + \vec{F}_{\text{in}}^{(0)} + \vec{F}_{\text{in}}^{(A)}$$

(determina la cantitate)

$$\vec{F}_{\text{in}}^{(0)} = \frac{1}{16\pi} t_2 F^2 = a_0 t_2 F^2$$

$$\vec{F}_{\text{in}}^{(A)} = a \left( t_2 F^2 \right)^2 + b \left( t_2 F^4 \right)$$

$$a = - \frac{5}{180} \frac{e^4}{m^4} \frac{1}{(4\pi)^3}$$

$$b = \frac{14}{180} \frac{e^4}{m^4} \frac{1}{(4\pi)^3}$$

calculam si cămp:

$$\frac{\Delta \vec{F}_{\text{tot}}}{\Delta A_F} = - \frac{1}{\Delta x_F} \left\{ \frac{\Delta \vec{F}_{\text{tot}}}{\Delta (\Delta A_F)} \right\} = 0$$

calculam i juri törnii:

$$\frac{\Delta t_2 F^2}{\Delta (\Delta A_F)} = - 2 \vec{F}_{\alpha \beta} \quad ; \quad \frac{\Delta (t_2 F^2)^2}{\Delta (\Delta A_F)} = 2 t_2 F^2 \frac{\Delta t_2 F^2}{\Delta (\Delta A_F)} = - 8 (t_2 F^2) \vec{F}_{\alpha \beta}$$

$$\frac{\Delta t_2 F^4}{\Delta (\Delta A_F)} = - 8 F_{\alpha \gamma} F_{\alpha \delta} F_{\beta \gamma} F_{\beta \delta}$$

$\Rightarrow$  RUTDO

$$1) \frac{\Delta_{\text{tot}} F}{\Delta(\Delta A_F)} = \frac{\Delta_{\text{RPP}} F_{\text{RPP}}}{\Delta(\Delta A_F)} = \frac{\Delta}{\Delta(\Delta A_F)} \left\{ (\Delta_H A_P - \Delta_\nu A_H) (\Delta_P A_H - \Delta_H A_P) \right\} =$$

$$= (S_{\mu_2} S_{\nu_P} - S_{\nu_2} S_{\mu_P}) (\Delta_P A_H - \Delta_H A_P) + (\Delta_{\nu_1} A_P - \Delta_H A_P) (S_{\mu_2} S_{\mu_P} - S_{\nu_1} S_{\nu_P}) \\ = (\bar{F}_{\mu_2} - \bar{F}_{\nu_P}) + (\bar{F}_{\nu_2} - \bar{F}_{\mu_P}) = -4 \bar{F}_{\mu_P}$$

$$2) \frac{\Delta_{\text{tot}} F^4}{\Delta(\Delta A_F)} = \frac{\Delta}{\Delta(\Delta A_F)} \left\{ (\Delta_H A_P - \Delta_\nu A_H) (\Delta_P A_\nu - \Delta_\nu A_P) (\Delta_\nu A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_\nu) (\Delta_{\bar{\nu}} A_H - \Delta_H A_{\bar{\nu}}) \right\}$$

$$= (S_{\mu_2} S_{\nu_P} - S_{\nu_2} S_{\mu_P}) (\Delta_\nu A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_\nu) (\Delta_{\bar{\nu}} A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_{\bar{\nu}}) + \\ + (\Delta_H A_P - \Delta_\nu A_H) (S_{\nu_2} S_{\bar{\nu}_P} - S_{\bar{\nu}_2} S_{\nu_P}) (\Delta_{\bar{\nu}} A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_{\bar{\nu}}) (\Delta_{\bar{\nu}} A_H - \Delta_H A_{\bar{\nu}}) + \\ + (\Delta_H A_P - \Delta_\nu A_H) (\Delta_\nu A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_\nu) (S_{\bar{\nu}_2} S_{\bar{\nu}_P} - S_{\bar{\nu}_2} S_{\nu_P}) (\Delta_{\bar{\nu}} A_H - \Delta_H A_{\bar{\nu}}) + \\ + (\Delta_H A_P - \Delta_\nu A_H) (\Delta_{\bar{\nu}} A_{\bar{\nu}} - \Delta_{\bar{\nu}} A_{\bar{\nu}}) (S_{\bar{\nu}_2} S_{\mu_P} - S_{\mu_2} S_{\bar{\nu}_P}) = \\ = (F_{\mu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\mu_2} - F_{\nu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\nu_2}) + (F_{\mu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\mu_2} - F_{\nu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\nu_2}) + \\ + (F_{\mu_2} F_{\nu_P} - F_{\nu_P} F_{\mu_2} - F_{\mu_2} F_{\nu_P} - F_{\nu_P} F_{\mu_2}) + (F_{\nu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\nu_2} - F_{\nu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\nu_2}) = \\ = (-2 F_{\mu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\mu_2}) + (-2 F_{\nu_2} F_{\bar{\nu}_2} - F_{\bar{\nu}_2} F_{\nu_2}) + (-2 F_{\mu_2} F_{\nu_P} - F_{\nu_P} F_{\mu_2}) + (-2 F_{\nu_2} F_{\nu_P} - F_{\nu_P} F_{\nu_2})$$

(2)

$$\frac{\Delta \dot{Q}_{\text{tot}}}{\Delta A_p} = \frac{1}{16\pi} \frac{\Delta E_F^2}{\Delta A_p} - \frac{5}{180} \frac{e^4}{m^4} \frac{1}{(4\pi)^3} \frac{\Delta (E_F p)^2}{\Delta A_p} + \frac{14}{180} \frac{e^4}{m^4} \frac{1}{(4\pi)^3} \frac{\Delta Q_F^4}{\Delta A_p}$$

$$= - \frac{1}{4\pi} \left\{ F_{\alpha\beta} - \frac{5}{90} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}_F p)^2 \bar{F}_{\alpha\beta} + \frac{14}{90} \frac{e^4}{m^4} \frac{1}{4\pi^2} F_{\alpha\beta} \bar{F}_{\delta\sigma} \bar{F}_{\delta\beta} \right\}$$

~~Dot com l'guna zonni~~

$$\left[ \frac{\Delta}{\Delta X_2} \left\{ F_{\beta\alpha} - \frac{5}{90} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}_F p)^2 \bar{F}_{\beta\alpha} + \frac{14}{90} \frac{e^4}{m^4} \frac{1}{4\pi^2} \bar{F}_{\beta\alpha} F_{\delta\sigma} \bar{F}_{\delta\alpha} \right\} - 4\pi T_R \right] = 0 \quad (2)$$

Ricci tensor cut o  $\bar{E} \times \bar{F}^2 = 2(\bar{E}^2 - H^2)$

$$\rho_{04} \quad \rho = 24$$

$$G_{04} = 0 \quad \Sigma_4 = 0$$

$$\frac{\Delta}{\Delta X_1} \left\{ F_{41} - \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}^2 - H^2) \bar{F}_{41} + \frac{14}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} \bar{F}_{41} F_{\delta\sigma} \bar{F}_{\delta1} \right\}$$

$$+ \frac{\Delta}{\Delta X_2} \left\{ F_{42} - \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}^2 - H^2) \bar{F}_{42} + \frac{14}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} \bar{F}_{42} F_{\delta\sigma} \bar{F}_{\delta2} \right\}$$

$$+ \frac{\Delta}{\Delta X_3} \left\{ F_{43} - \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}^2 - H^2) \bar{F}_{43} + \frac{14}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} \bar{F}_{43} F_{\delta\sigma} \bar{F}_{\delta3} \right\}$$

$$+ \frac{\Delta}{\Delta X_4} \left\{ \frac{7}{45} \frac{e^4}{m^4} \frac{1}{4\pi^2} (\bar{E}^2 - H^2) \bar{F}_{44} + \underbrace{F_{\alpha\beta} \bar{F}_{\delta\sigma} \bar{F}_{\delta\beta}}_0 = 24 \pi \alpha'$$

desarrollo (4a):

$$F_{4x} F_{8z} \bar{F}_{6z} = i \left\{ (H_3 H_1) \hat{E}_1 + (H_2 H_2) \hat{E}_2 + (H_3 H_3) \hat{E}_3 + (\hat{E}^2 - H^2) \hat{E}_2 \right\}$$

$$F_{4x} F_{8z} \bar{F}_{6z} = i \left\{ (H_2 H_1) \hat{E}_1 + (H_2 H_2) \hat{E}_2 + (H_2 H_3) \hat{E}_2 + (\hat{E}^2 - H^2) \hat{E}_2 \right\}$$

$$F_{4x} F_{8z} \bar{F}_{6z} = i \left\{ (H_1 H_1) \hat{E}_1 + (H_1 H_2) \hat{E}_2 + (H_1 H_3) \hat{E}_2 + (\hat{E}^2 - H^2) \hat{E}_1 \right\}$$

dado:

$$\cancel{\cancel{\frac{\partial}{\partial X_1}}} \left\{ \hat{E}_2 = \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} (\hat{E}^2 - H^2) \hat{E}_2 + \frac{2}{45} \frac{e^4}{m^4} \cdot \frac{1}{4\bar{a}^2} [ (H_1 H_1) \hat{E}_1 + (H_1 H_2) \hat{E}_2 + (H_1 H_3) \hat{E}_2 + (\hat{E}^2 - H^2) \hat{E}_1 ] + \right.$$

$$\cancel{\cancel{\frac{\partial}{\partial X_2}}} \left\{ \hat{E}_2 = \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} (\hat{E}^2 - H^2) \hat{E}_2 + \frac{2}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} [ (H_2 H_1) \hat{E}_1 + (H_2 H_2) \hat{E}_2 + (H_2 H_3) \hat{E}_2 + (\hat{E}^2 - H^2) \hat{E}_1 ] + \right.$$

$$\cancel{\cancel{\frac{\partial}{\partial X_3}}} \left\{ \hat{E}_2 = \frac{5}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} (\hat{E}^2 - H^2) \hat{E}_2 + \frac{2}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} [ (H_3 H_1) \hat{E}_1 + (H_3 H_2) \hat{E}_2 + (H_3 H_3) \hat{E}_2 + (\hat{E}^2 - H^2) \hat{E}_1 ] \right\} =$$

$$= \frac{5}{2X_1} \left\{ \hat{E}_1 + \frac{1}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} [ 2(\hat{E}^2 - H^2) \hat{E}_1 + 7[(H_1 H_1) \hat{E}_1 + (H_1 H_2) \hat{E}_2 + (H_1 H_3) \hat{E}_2] ] \right\} + \\ + \frac{2}{2X_2} \left\{ \hat{E}_2 + \frac{1}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} [ 2(\hat{E}^2 - H^2) \hat{E}_2 + 7[(H_2 H_1) \hat{E}_1 + (H_2 H_2) \hat{E}_2 + (H_2 H_3) \hat{E}_2] ] \right\} + \\ + \frac{2}{2X_3} \left\{ \hat{E}_3 + \frac{1}{45} \frac{e^4}{m^4} \frac{1}{4\bar{a}^2} [ 2(\hat{E}^2 - H^2) \hat{E}_3 + 7[(H_3 H_1) \hat{E}_1 + (H_3 H_2) \hat{E}_2 + (H_3 H_3) \hat{E}_2] ] \right\} = 2m_1$$

(3)

da cui definiamo le vettori

$$\Delta_i = \dot{e}_{in} \dot{e}_{in}$$

con

$$e_{in} = \sin + \frac{1}{45} \frac{\rho^4}{m^4} \frac{1}{4\pi^2} \left[ 2(\bar{E}^2 - H^2) \sin + 7H_1 H_2 \right]$$

AVERO

$$\frac{\Delta_1}{\Delta x_1} + \frac{\Delta_2}{\Delta x_2} + \frac{\Delta_3}{\Delta x_3} = 2\pi f \Rightarrow$$

$$\vec{\nabla} \cdot \vec{\Delta} = 4\pi f$$

ANALOGAMENTE

PER LA (2)

PER R=1, VIZ. DEFINIZIONE (VETTORE SOTTRAZIONE)

$$\Delta_i = \mu_{in} H_u$$

con

$$\mu_{in} = \sin + \frac{1}{45} \frac{\rho^4}{m^4} \frac{1}{4\pi^2} \left[ 2(\bar{E}^2 - H^2) \sin - 7G_1 G_2 \right]$$

MUSONE

LOWK LOWK

$$\vec{\nabla} \cdot \vec{B} = \frac{1}{c} \frac{\Delta}{\Delta t} + \frac{4\pi}{c} \frac{\vec{J}}{\Delta t}$$

NOTA: PER  $\beta=1$

$$\frac{\Delta}{\Delta x^2} \left\{ F_{12} - \frac{5}{50} \frac{\rho^4}{m^4} \frac{3}{4\pi^2} 2(E^2 - H^2) F_{12} + \frac{14}{50} \frac{\rho^4}{m^4} \frac{1}{4\pi^2} F_{12} F_{23} F_{32} \right\} = 4\pi \frac{\rho}{c} V_1$$

ISSIMO

$$\begin{cases} F_{12} F_{23} F_{32} = (\bar{E}^2 - H^2) H_2 - (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_3 \\ F_{12} F_{32} \bar{F}_{23} = -\left\{ (\bar{E}^2 - H^2) H_2 - (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_2 \right\} \\ F_{12} F_{23} \bar{F}_{32} = -i \left\{ (\bar{E}^2 - H^2) \bar{E}_1 + (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) H_1 \right\} \end{cases}$$

da cui:

$$\frac{\partial}{\partial x^2} \left\{ H_3 + \frac{c^4}{45} \frac{1}{m^4} (\bar{E}^2 - H^2) H_2 + \frac{7}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ (\bar{E}^2 - H^2) H_3 - (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_3 \right] \right\} . \quad (5)$$

$$= \frac{\partial}{\partial x^3} \left\{ H_2 - \frac{5}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} (\bar{E}^2 - H^2) H_2 + \frac{7}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ (\bar{E}^2 - H^2) H_2 - (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_2 \right] \right\}$$

$$- \frac{\partial}{\partial c} \frac{\partial}{\partial t} \left\{ \bar{E}_1 - \frac{5}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} (\bar{E}^2 - H^2) \bar{E}_1 + \frac{7}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ (\bar{E}^2 - H^2) \bar{E}_1 + (\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) H_1 \right] = 4\bar{u} \frac{\partial}{\partial c} V_1 \right.$$

da cui

$$\frac{\partial}{\partial x^2} \left\{ H_3 + \frac{1}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ 2(\bar{E}^2 - H^2) H_2 - 7(\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_3 \right] \right\}$$

$$- \frac{\partial}{\partial x^3} \left\{ H_2 + \frac{1}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ 2(\bar{E}^2 - H^2) H_2 - 7(\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) \bar{E}_2 \right] \right\} =$$

$$= 4\bar{u} \frac{\partial}{\partial c} V_1 + \frac{1}{c} \frac{\partial}{\partial t} \left\{ \bar{E}_1 + \frac{1}{45} \frac{c^4}{m^4} \frac{1}{4\bar{u}^2} \left[ 2(\bar{E}^2 - H^2) \bar{E}_1 + 7(\bar{E}_1 H_1 + \bar{E}_2 H_2 + \bar{E}_3 H_3) H_1 \right] \right\}$$

Poi:

$$\left( \frac{\partial \beta_2}{\partial x^2} - \frac{\partial \beta_2}{\partial x^3} \right) = 4\bar{u} \frac{\partial V_1}{\partial c} + \frac{1}{c} \frac{\partial}{\partial t} D_1 \Rightarrow (\nabla \wedge \beta)_2 = 4\bar{u} \frac{\partial V_1}{\partial c} + \frac{1}{c} \frac{\partial D_1}{\partial t}$$

considerando i casi  $\beta_2 = 2, 3$  avendo l'interpretazione vettoriale

essendo

$$\beta_1 = H_1 \wedge H_2$$

$$\boxed{(\nabla \wedge \beta) = \frac{4\bar{u}}{c} \frac{\partial V_1}{\partial c} + \frac{1}{c} \frac{\partial D_1}{\partial t}}$$